

# Re-exam Makrok 2

~~11/10-10~~  
3/2-2012

~~$E_t = C_t - 201t$~~

1)

a) (\*) is essentially just national product accounting:

$$\dot{K} = Y - c_t - \delta K$$

(\*\*) is the U-R rule expressed in terms of  $\bar{\theta} \equiv c_t/Y$  and using that in equilibrium,  $r_t = f'(k_t) - \delta$ .

(\*\*\*) is the TVC expressed in terms of  $\tilde{a}_t \equiv a_t/Y_t = \frac{A_t}{Y_t L_t} = \frac{K_t}{Y_t L_t} \equiv \bar{k}_t$ .

$\delta$  = cap. deprec. rate

$\eta$  = rate of technical progress

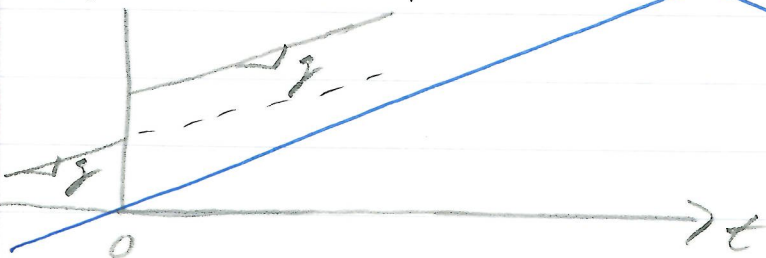
$n$  = population growth rate

$\theta$  = elast. of marg. utility of cons.  
(derive for cons. smoothing)

$\rho$  = pure rate of time preference  
(rate of impatience)

b) see p. 338. <sup>Yes,</sup> divergent paths don't satisfy TVC.

c)  $T_0 \rightarrow T'_0 > T_0$ ,  $\eta$  unchanged  
 $\ln T$                        $\ln T'$



b) At time  $t$  the firm solves

$$\max_{K, L} \pi = F(K, TL) - (r+\delta)K - wL$$

FOC's:

$$\frac{\partial \pi}{\partial K} = F_K(K, TL) - (r+\delta) = 0 \quad (1)$$

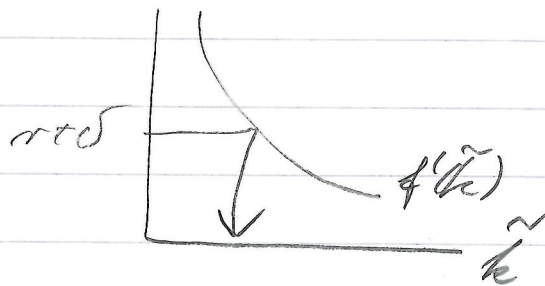
$$\frac{\partial \pi}{\partial L} = F_L(K, TL)T - w = 0 \quad (2)$$

The desired capital-labor ratio,  $k \equiv K/L$ , is found the following way:

$$Y = F(K, TL) = TL F(\tilde{k}, 1) \equiv TL f(\tilde{k}),$$

where  $f' = F_K > 0$ ,  $f'' < 0$ . So (1)  $\Rightarrow$

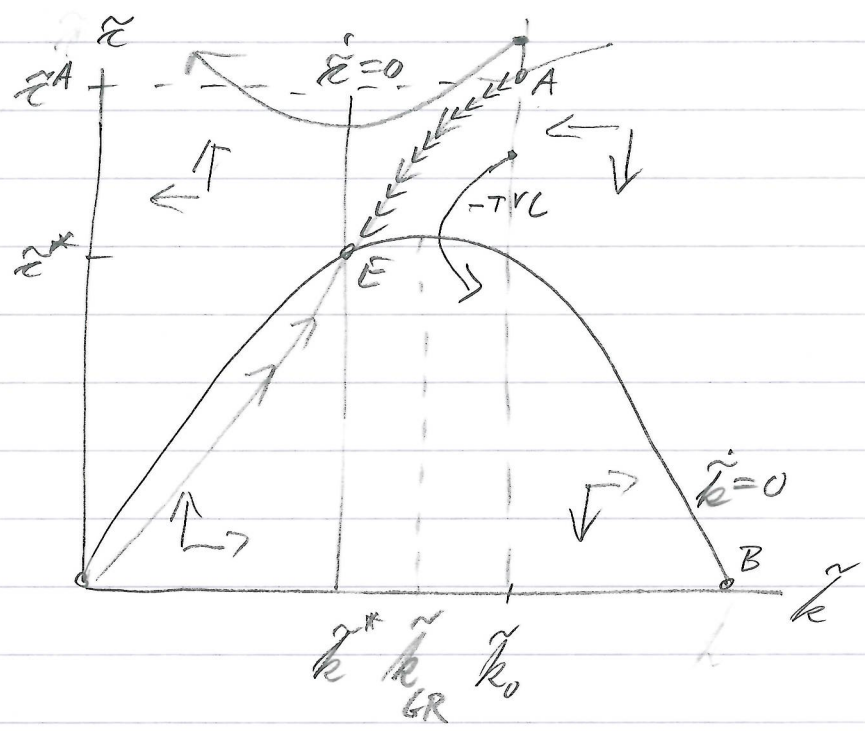
$$f'(\tilde{k}) = r + \delta$$



$$k = \tilde{k} \cdot T$$

c)  $\dot{\tilde{k}} \geq 0$  for  $\tilde{c} \leq f'(\tilde{k}) - (\delta + \rho + n)\tilde{k}$

$\dot{\tilde{c}} = 0$  for  $\tilde{c} = 0$  and  $f'(\tilde{k}) - \delta = \rho + \theta g$   
 i.e.,  $\tilde{k} = \tilde{k}^*$  when  $f'(\tilde{k}^*) = \delta + \rho + \theta g$   
 $\dot{\tilde{c}} \geq 0$  for  $\tilde{c} > 0$  and  $\tilde{k} \leq \tilde{k}^*$



We know that  $f(0) \geq 0$ . The phase diagram, as drawn here, represents the case  $f(0) = 0$ .

At time  $t=0$  the economy,  $(\tilde{k}, \tilde{c})$ , must be at some point at the line  $\tilde{k} = \tilde{k}_0$  since  $\tilde{k}_0$  is pre-determined.

The steady state,  $E$ , is seen to be a saddle point. At time  $t=0$  general equilibrium with perfect foresight

requires that the economy is at the point A (the crossing point of the line  $\tilde{k} = \tilde{k}_0$  and the saddle path), i.e.,  $\tilde{\epsilon}_0 = \tilde{\epsilon}^A$  is required.

If  $\tilde{\epsilon}_0 < \tilde{\epsilon}^A$ , the generated evolution of  $(\tilde{k}, \tilde{\epsilon})$  will be diverging and not satisfy the TVC of the households.

If  $\tilde{\epsilon}_0 > \tilde{\epsilon}^A$ , — 4 —

..... not satisfy the NPG of the households.

Hence, the divergent paths can be ruled out as equilibrium paths with perfect foresight.

We are left with the convergent path AE along the saddle path as the solution. Indeed, this path satisfies the TVC, (3), since it gives  $\tilde{k}_t \rightarrow \tilde{k}^*$  for  $t \rightarrow \infty$  so that

$$\lim_{t \rightarrow \infty} \tilde{k}_t e^{-\rho t} - \int_0^t (\dot{f}(\tilde{k}_s) - \delta - g - n) ds$$

$$= \tilde{k}^* e^{-\rho t} - [f(\tilde{k}^*) - \delta - g - n] t = 0$$

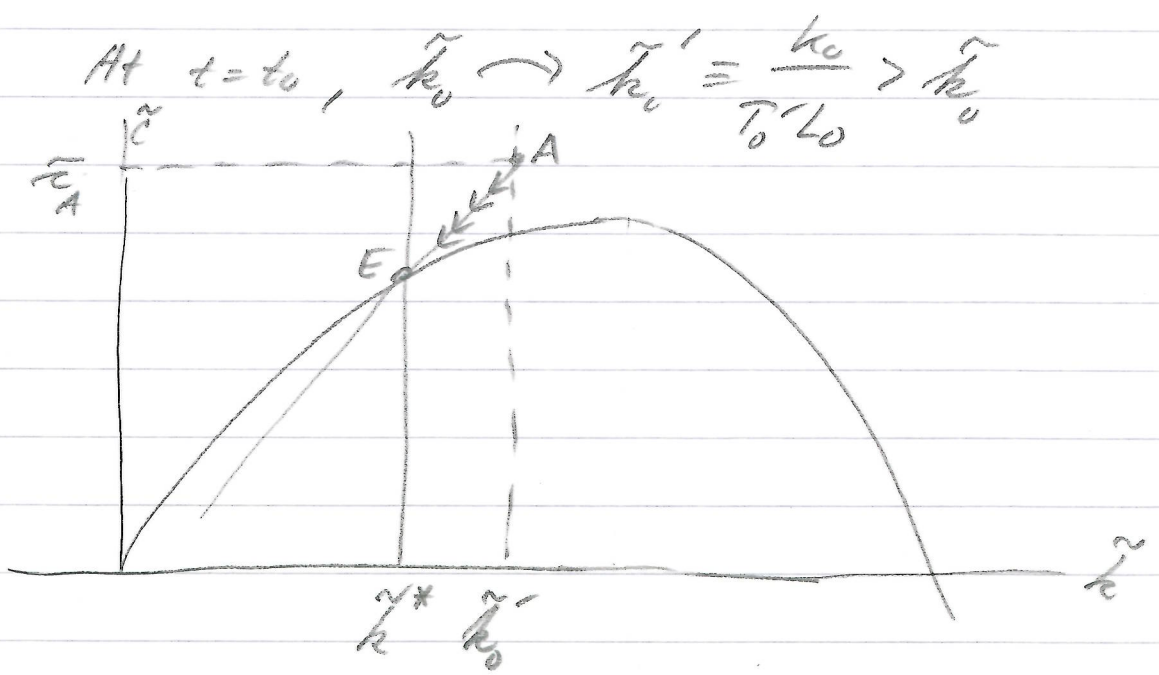
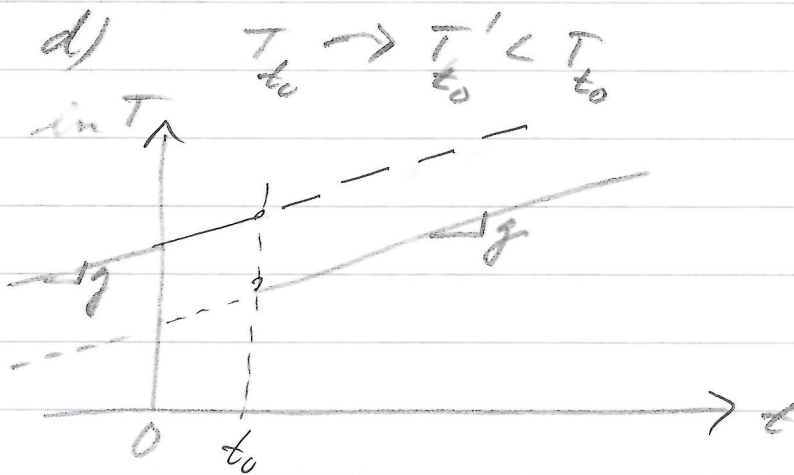
in view of  $f'(\tilde{k}^*) - \delta = p + \theta g > g + n$ ,  
 an inequality following from  
 the condition

$$p - n > (1 - \theta)g,$$

which is equivalent with

$$p + \theta g > g + n.$$

$$[f'(\tilde{k}_{GR}) - \delta = g + n, \text{ so } \tilde{k}^* < \tilde{k}_{GR}]$$



The economy jumps to the point A and then moves back along the saddle path for  $t \rightarrow \infty$ .

$$\tilde{k}_t \rightarrow \tilde{k}^* \text{ and } \tilde{c}_t \rightarrow \tilde{c}^* \text{ for } t \rightarrow \infty.$$

$$e) r_t = f'(\tilde{k}_t) - \delta \downarrow \text{ at } t = t_0$$

$$r_t \rightarrow f'(\tilde{k}^*) - \delta \equiv r^* \text{ for } t \rightarrow \infty.$$

$$f) w_t = \frac{\partial Y_t}{\partial L_t} = F_L(k_t, T_t) T_t$$

$$= [f(\tilde{k}_t) - \tilde{k}_t f'(\tilde{k}_t)] T_t \equiv \tilde{w}(\tilde{k}_t) T_t$$

$$\tilde{w}'(\tilde{k}) = f'(\tilde{k}) - (\tilde{k} f''(\tilde{k}) + f'(\tilde{k}))$$

$$= -\tilde{k} f''(\tilde{k}) > 0$$

$$\text{so } w_{t_0}' = \tilde{w}(\tilde{k}_{t_0}') > \tilde{w}(\tilde{k}_{t_0}),$$

$$\text{but } T_0' < T_0$$

So there are two opposing effects on  $w_t$  at time  $t = t_0$ .

$$g) w_t = \tilde{w}(k_t) T_t \rightarrow \tilde{w}(k_t^*) T_t' \text{ for } t \rightarrow \infty$$

$$\text{where } T_t' = T_{t_0}' e^{\int_{t_0}^t g(t-t_0)} < T_{t_0} e^{\int_{t_0}^t g(t-t_0)}$$

So in the long run  $w_t$  will necessarily be lower due to the negative technology shock.

$$h) \theta = 1. \quad c_t = (p-n)(a_t + h_t) = (p-n)(k_t + h_t)$$

$$\text{where } h_t = \int_t^{\infty} w_s e^{-\int_t^s (r_t - n) dt} ds$$

At  $t = t_0$ ,  $h_t$  changes:

$$h_t' < h_t \text{ for } t > t_0,$$

$$\text{but also } w_t' < w_t.$$

Hence impact effect on  $c$  ambiguous.

Alternative reasoning, less deep:

$$c_t' \equiv \tilde{c}_t' T_t', \text{ where } \tilde{c}_t' > \tilde{c}_t \text{ for } t > t_0$$

$$\text{but } T_t' < T_t \text{ for } t > t_0.$$



2)

a)

$$\max_{(L_t, I_t)_{t=0}^{\infty}} V_0 = \int_0^{\infty} \left[ k_t^\alpha (TL)^{1-\alpha} - w_t L_t - I_t - \beta \frac{I_t^2}{2k_t} \right] e^{-rt} dt$$

s.t.

$$L_t \geq 0, \quad I_t \text{ free}$$

$$\dot{K}_t = I_t - \delta k_t, \quad k_0 > 0$$

$$k_t \geq 0 \quad \forall t \geq 0$$

$$H = k_t^\alpha (TL)^{1-\alpha} - wL - I - \beta \frac{I^2}{2k} + \lambda (I - \delta k)$$

b)

$$\frac{\partial H}{\partial L} = (\alpha - 1) k^\alpha T^{1-\alpha} L^{-\alpha} - w = 0 \tag{1}$$

$$\frac{\partial H}{\partial I} = -1 - \beta \frac{I}{k} + \lambda = 0 \tag{2}$$

$$\frac{\partial H}{\partial k} = \alpha k^{\alpha-1} (TL)^{1-\alpha} + \beta \frac{I^2}{2k^2} - \lambda \delta = \lambda \delta - \lambda \tag{3}$$

$$TVC: \lim_{t \rightarrow \infty} k_t \lambda_t e^{-rt} = 0 \tag{TVC}$$

$$\Rightarrow I = \frac{q-1}{\beta} k$$

$$c) (2) \Rightarrow 1 + \beta \frac{I}{k} = q \Rightarrow \frac{I}{k} = \frac{1}{\beta} (q-1) \checkmark$$

$$MC = MB$$

So  $q$  is the value to the firm of the marginal unit of installed capital along the optimal path. Hence,  $q$  is the shadow price of installed capital.

From now, SOE

d) For  $t \geq t_0$

$$R_t = k_t^\alpha (T_t L_t)^{1-\alpha} - w_t L_t - (1-\sigma)I_t - \beta \frac{I_t^2}{2k_t}$$

So (2) is changed into

$$-(1-\sigma) - \beta \frac{I}{k} + q = 0 \Rightarrow$$

$$1-\sigma + \beta \frac{I}{k} = q \Rightarrow$$

$$\beta \frac{I}{k} = q + \sigma - 1 \Rightarrow$$

$$\frac{I}{k} = \frac{1}{\beta} (q + \sigma - 1)$$

So  $\sigma \uparrow \Rightarrow \frac{I}{k} \uparrow$  for any given  $q$ .

$$\tilde{k}_t \equiv \frac{k_t}{L_t}, \quad L_t = L_0 e^{nt}$$

$$\frac{\dot{\tilde{k}}}{\tilde{k}} = \frac{\dot{k}}{k} - (\delta + n) = \frac{I - \delta k}{k} - (\delta + n)$$

$$= \frac{I}{k} - (\delta + \delta + n) = \frac{1}{\beta} (\eta + \sigma - 1) - (\delta + \delta + n)$$

$$\Rightarrow \dot{\tilde{k}} = \left[ \frac{1}{\beta} \eta + \frac{\sigma - 1}{\beta} - (\delta + \delta + n) \right] \tilde{k}$$

$$\Rightarrow \dot{\tilde{k}} = \left[ \frac{1}{\beta} \eta - (\delta + \delta + n + \frac{1 - \sigma}{\beta}) \right] \tilde{k}$$

$$\equiv (a\eta - b) \tilde{k}$$

f) (3)  $\Rightarrow$

$$\dot{g} = (\sigma + \delta)g - \alpha \tilde{k}^{\alpha-1} - \frac{\beta}{2} \left( \frac{I}{k} \right)^2$$

$$= (\sigma + \delta)g - \alpha \tilde{k}^{\alpha-1} - \frac{\beta}{2} \frac{1}{\beta^2} (\eta + \sigma - 1)^2$$

$$= (\sigma + \delta)g - \frac{(\eta + \sigma - 1)^2}{2\beta} - \alpha \tilde{k}^{\alpha-1}$$

g)  $r > \delta + n$

$$\dot{\tilde{k}} = 0 \text{ for } \tilde{k} = 0 \text{ or } g = \beta(\delta + \delta + n) + 1 - \sigma \equiv g^*$$

$$\dot{\tilde{k}} > 0 \text{ for } \tilde{k} > 0 \text{ and } g \geq \beta(\delta + \delta + n) + 1 - \sigma = g^*$$

$$\dot{q} \stackrel{>}{<} 0 \text{ for } (r+\delta)q - \frac{(\beta+\delta-1)^2}{2\beta} \stackrel{>}{<} \alpha \tilde{k}^{1-\alpha} \quad (4)$$

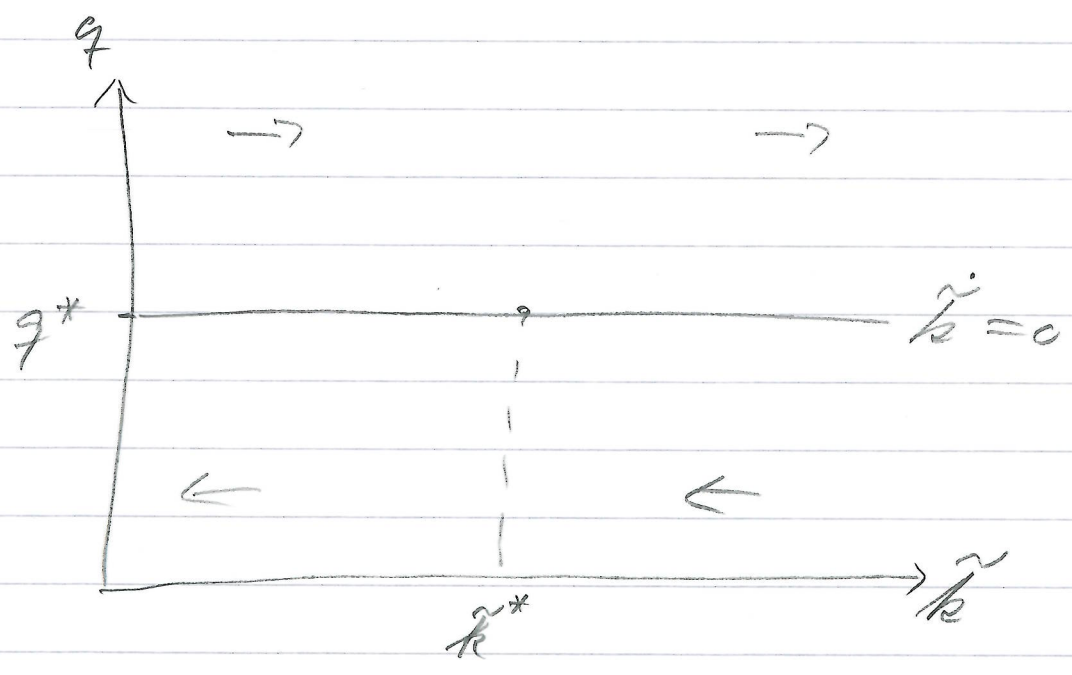
In st. st.  $\dot{\tilde{k}} = 0 = \dot{q}$

i.e.,  $q = q^*$  and  $\tilde{k} = \tilde{k}^*$

$$\begin{aligned} \text{where } \alpha \tilde{k}^{* \alpha-1} &= (r+\delta)q^* - \frac{(\beta+\delta-1)^2}{2\beta} \\ &= (r+\delta)[\beta(\delta+\delta+m)+1-\delta] - \frac{[\beta(\delta+\delta+m)]^2}{2\beta} \end{aligned}$$

hence

$$\tilde{k}^* = \left\{ \frac{(r+\delta)[\beta(\delta+\delta+m)+1-\delta] - \frac{\beta(\delta+\delta+m)^2}{2}}{\alpha} \right\}^{\frac{1}{1-\alpha}}$$



To draw the  $\dot{q} = 0$  curve we need information about its slope.

$$(4) \Rightarrow (r+\delta)z - \frac{(z+\delta-1)^2}{2\beta} - \alpha k^{\alpha-1} = 0 \quad (5)$$

i.e.,  $\varphi(\tilde{k}, \tilde{z}) = 0 \quad (5')$

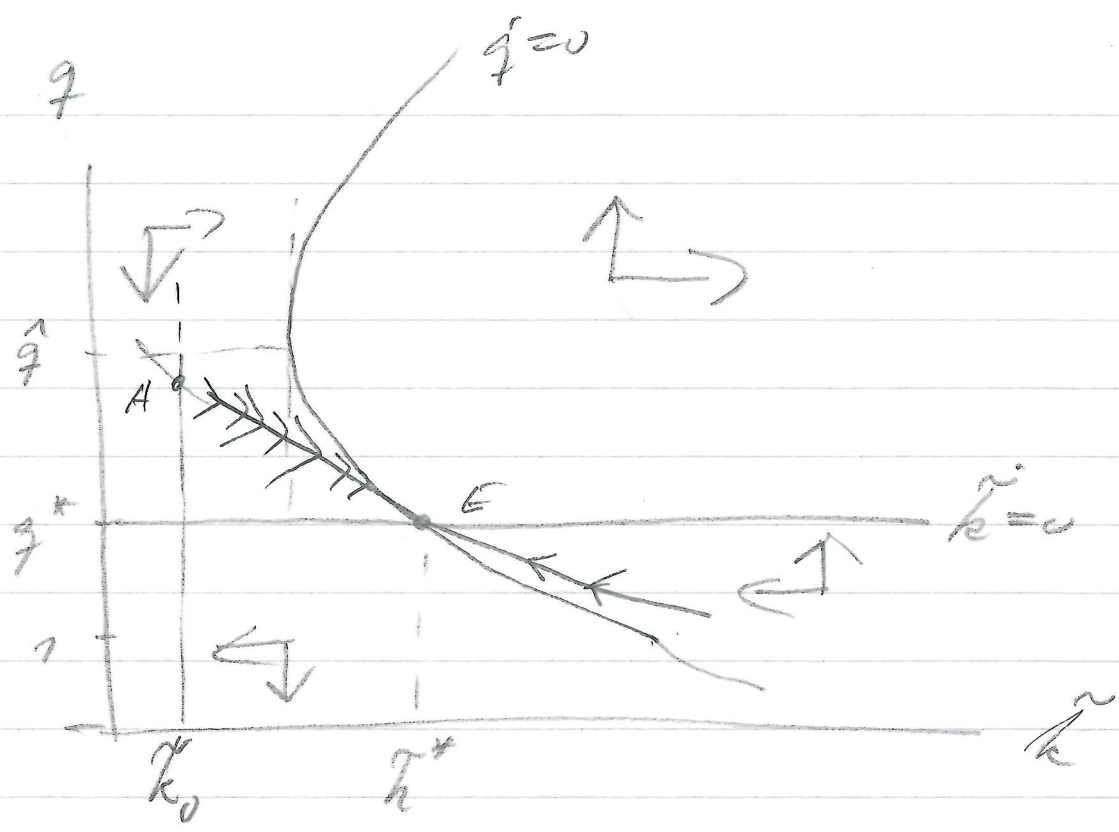
We have  $\varphi(\tilde{k}^*, \tilde{z}^*) = 0$

For  $(\tilde{k}, \tilde{z})$  close to  $(\tilde{k}^*, \tilde{z}^*)$ , (5') defines  $\tilde{z}$  implicitly as a function  $\tilde{z} = \psi(\tilde{k})$  where

$$\begin{aligned} \psi'(\tilde{k}) &= - \frac{\frac{\partial \varphi}{\partial \tilde{k}}}{\frac{\partial \varphi}{\partial \tilde{z}}} = + \frac{\alpha(\alpha-1)\tilde{k}^{\alpha-2}}{r+\delta - \frac{z+\delta-1}{\beta}} \\ &= \frac{\alpha(\alpha-1)\tilde{k}^{\alpha-2}}{\frac{z+\delta-1}{\beta} - (r+\delta)} \\ &\approx \frac{\alpha(\alpha-1)\tilde{k}^{*\alpha-2}}{\frac{z^*+\delta-1}{\beta} - (r+\delta)} \quad (\text{for } \tilde{k} \approx \tilde{k}^*) \\ &= \frac{\alpha(\alpha-1)\tilde{k}^{*\alpha-2}}{\delta+\delta+m - (r+\delta)} < 0 \end{aligned}$$

since  $r > \delta+m$ .

Phase diagram: see p. 6.  
The arrows indicate that the st. st. is a saddle point.



$$\hat{q} = \frac{\hat{q} + \sigma - 1}{\beta} = \nu + \delta \Rightarrow$$

$$\hat{q} = \beta(\nu + \delta) + 1 - \sigma$$

$$q > \hat{q} \Rightarrow \frac{dq}{dk} \Big|_{\dot{q}=0} > 0$$

At  $t=0$  the system will be at some point on the line  $k = k_0$  since  $k_0$  is pre-determined.

The economy will over time move along the saddle path towards the stab. E. This evolution satisfies (TVC). The divergent paths do not.

3)

a) True. Let  $T = T_0 e^{gt}$ ,  $g > 0$

If  $Y = k^\alpha (TL)^{1-\alpha}$ , there is Harrod-neutral technical progress.

Define  $B = T^\alpha$ , then  $Y = B k^\alpha L^{1-\alpha}$  and so there is also Hicks-neutral.

Define  $X = T^{\frac{1-\alpha}{\alpha}}$ , then  $Y = (Xk)^\alpha L^{1-\alpha}$  and so there is also Solow-neutral.

analogue

The same argument goes through if we start from Hicks-neutral or Solow neutral.

b) The IBC of the government is the budget constraint

$$\sum_{t=0}^{\infty} \underbrace{(G_t + X_t)}_{\text{spending}} (1+r)^{-(t+1)} \leq \sum_{t=0}^{\infty} \underbrace{T_t}_{\text{gross tax revenue}} (1+r)^{-(t+1)} - B_0$$

$B_0$  = government debt at the beginning of period 0.

The statement is false. The claimed

"only if" does not hold if  $r \leq q_1$

and the claimed "if" does not

hold if  $1 + q_1 < \lim_{t \rightarrow \infty} \frac{B_{t+1}}{B_t} < 1 + r$

c) In Problem 2 there are strictly convex capital installation costs. Then the firm has to take the whole future into account in its investment decision.

In Problem 1 there are no installation costs and the firm's intertemporal value maximization problem can be reduced to a series of static profit maximization problems.